Pairing Mixers with Reflectionless Filters to Improve System Performance (AN-75-007)

I. INTRODUCTION

Traditional filter designs employ circuits which reject undesired signals by reflecting them back to the source. There are many applications in which these reflections produce intermodulation products, gain ripples and other problems in system performance. Non-linear devices such as mixers respond to out-of-band frequencies and are highly sensitive to the reflections caused by conventional filter designs. This becomes especially challenging as filters are often needed near or adjacent to mixers to better define bandwidth or suppress unwanted harmonics.

While RF system designers have used several bruteforce approaches to manage these adverse effects such as inserting attenuators or isolation amplifiers around sensitive components, these techniques are known to degrade overall system signal-to-noise ratio (SNR) and dynamic range. Absorption of stop band signals has been achieved by terminating one port of a diplexer (or all but one port of a multiplexer), but this approach is demanding on space requirements and still results in some reflections due to mismatch in the transition. Balanced filters with quadrature hybrids at the input and output can also be used to buffer the circuit from reflective elements, but the bandwidth of the filter is then limited by that of the hybrids used, which makes this technique unsuitable for broadband applications.

To support a clear and prevalent need to eliminate reflections from filters in the stop band, Mini-Circuits' has developed the patented X-series of reflectionless filters. These filters employ a novel filter topology in which undesired signals are fully absorbed and terminated internally and for which the reflection coefficient is zero for all frequencies.

II. THEORY: MINIMIZING REFLECTIONS TO IMPROVE DYNAMIC RANGE

Reflectionless filters are particularly useful for pairing with sensitive non-linear devices where traditional filters are often problematic. A prime example is the case in which a filter is used at the output of a mixer in the signal chain. Mixers generate spurious mixing products, higher LO harmonics, and other unwanted signal elements that must be filtered out. However, with a conventional filter,



Figure 1: Typical intermodulation expansion due to reflections from multiple filters

these spurious tones are reflected back into the mixer where they can convert again, or re-mix with the desired signals to create a multitude of un-intended signals that may fall within the desired passband.

Reducing intermodulation products produced by the non-linear mixer has always been a design goal, and the industry has had various levels of success with high dynamic range FET based mixers. However, even the best mixers produce intermodulation products at some level from each port which then react with the neighboring elements in the RF chain. When these adjacent elements are filters, the out-of-band intermodulation products are fully reflected back into the mixer to re-combine with the fundamental signal and produce additional "family members" of unwanted spurious products. These spurious products make their way to the output IF, and several end up in-band, limiting the overall dynamic range of the system.

When out-of-band reflections from filters are minimized, those "family member" spurious products are reduced, resulting in a net reduction of in-band unwanted



www.minicircuits.com P.O. Box 350166, Brooklyn, NY 11235-0003 (718) 934-4500 sales@minicircuits.com

intermodulation products and improvement in overall system dynamic range.



Figure 2: Typical intermodulation expansion due to reflections from multiple filters

III. PROOF OF CONCEPT

An application circuit was assembled and tests were performed to compare system performance when a mixer was paired with a conventional filter to performance when the same mixer was paired with a reflectionless filter.

Test 1: IF Output Reflection Spectrum with Single Input Frequency

The test setup shown in figure 3 was assembled and the reflection from the filter back to the output port of the mixer was measured in 3 cases for comparison:

Case 1: No filter at mixer output Case 2: Conventional filter at mixer output Case 3: Reflectionless filter at mixer output



Figure 3: Test block diagram for IF output reflection spectrum with single input frequency

The test results for each case are shown in figures 4 through 6. While the conventional filter reduces the reflections present when the mixer is used alone, the reflectionless filter virtually eliminates those reflections altogether. The reflected signal at 2 GHz exhibits a reduction of more than 30 dB from -34.35 dBm with the

conventional filter to -66.12 dBm when the reflectionless filter is used. The other reflected signals were similarly suppressed when the reflectionless filter was used.



Figure 4: IF output reflection spectrum without filter





Figure 5: IF output reflection spectrum with conventional filter

Figure 6: IF output reflection spectrum with reflectionless filter

Mini-Circuits*

www.minicircuits.com P.O. Box 350166, Brooklyn, NY 11235-0003 (718) 934-4500 sales@minicircuits.com

Test 2: IF Input Reflection Spectrum with Single Input Frequency

To measure the reflection through the mixer input back to the source, the test setup in Figure 7 was used. Again, 3 cases were tested:

Case 1: No filter at mixer output Case 2: Conventional filter at mixer output Case 3: Reflectionless filter at mixer output



Figure 7: Test block diagram for RF input reflection spectrum with single input frequency.

The difference in system performance when the reflectionless filter is used is less obvious in this test but still significant. While the nominal measurements of reflected signal before the mixer don't show a significant reduction in the reflection strength, they do show *greater consistency* with the input reflection characteristics of the mixer when no filter is used. This means that effects generated by the reflectionless filter at the output add or subtract minimally to the natural reflections from the mixer input port. This essentially results in much more predictable behavior at the mixer input.

We can best see this difference by looking at the delta between measured reflections of the mixer alone and the measurements when each type of filter is used at the output. These delta values are shown in table 1. Note the low variation when the reflectionless filter is used at the mixer output.

TABLE 1*		
Frequency	Δ (M _R - C _R)	Δ (M _R - R _R)
(GHz)	(dB)	(dB)
0.4	1.6	0.69
2.4	8.98	-6.87
2.8	-13.22	-6.4
4.0	-15.64	-0.07
4.4	23.58	-7.13
4.8	-14.57	-4.14
5.2	13.04	1.95
6.8	5.96	6.96
7.2	-22.5	5.76
7.6	15.97	13.11



Figure 8: RF input reflection spectrum without filter.



Figure 9: RF input reflection spectrum with conventional filter



Figure 10: RF input reflection spectrum with reflectionless filter

- * M_R = RF input reflection with mixer alone
- $C_R = RF$ input reflection with conventional filter
- $R_R = RF$ input reflection with reflectionless filter



www.minicircuits.com P.O. Box 350166, Brooklyn, NY 11235-0003 (718) 934-4500 sales@minicircuits.com

Test 3: Conversion Loss and IP3 Test (Sweeping RF and LO Frequencies)

The test setup in figure 11 was used to test the conversion loss and IP3. The RF1 signal was swept to test conversion loss. The RF2 signal was added to interfere with RF1 and test IP3. As in each of the previous tests, measurements were made for 3 cases:

Case 1: No filter at mixer output Case 2: Conventional filter at mixer output Case 3: Reflectionless filter at mixer output



Figure 11: Test block diagram for conversion loss and IP3 test.

Plots of conversion loss and input IP3 are shown in figures 12 and 13 respectively. The conversion loss plots show that when the mixer is paired with a conventional filter, the performance varies due to the reflected signal from the filter; at some frequencies the measured loss is greater than that of the mixer alone, and at other's it's less. When the reflectionless filter is used, the loss of the filter itself is added, but the variations seen with the conventional filter are eliminated, and performance closely follows that of the mixer alone.

Similarly, the IP3 tests show erratic behavior when the conventional filter is used. When the reflectionless filter is used, the IP3 performance tracks the natural performance of the mixer consistently. Both of these results again demonstrate more consistent and predictable system performance when the mixer is paired with the reflectionless filter.



Figure 12: Conversion loss plots for 3 test cases.



Figure 13: Input IP3 plots for 3 test cases.

IV. CONCLUSION

A comparison of system performance when a mixer is paired with a conventional filter versus a reflectionless filter shows that the reflectionless filter virtually eliminates reflections at the mixer output, dramatically improving system dynamic range. Additionally, more predictable reflection behavior is achieved at the mixer input, and conversion loss and IP3 conform closely to the performance of the mixer alone. These results suggest dramatic improvements in system performance can be achieved by pairing mixers with reflectionless filters in place of conventional filters.

IMPORTANT NOTICE

© 2015 Mini-Circuits

This document is provided as an accommodation to Mini-Circuits customers in connection with Mini-Circuits parts only. In that regard, this document is for informational and guideline purposes only. Mini-Circuits assumes no responsibility for errors or omissions in this document or for any information contained herein. Mini-Circuits may change this document or the Mini-Circuits parts referenced herein (collectively, the "Materials") from time to time, without notice. Mini-Circuits makes no commitment to update or correct any of the Materials, and Mini-Circuits shall have no responsibility whatsoever on account of any updates or corrections to the Materials or Mini-Circuits' failure to do so.

Mini-Circuits customers are solely responsible for the products, systems, and applications in which Mini-Circuits parts are incorporated or used. In that regard, customers are responsible for consulting with their own engineers and other appropriate professionals who are familiar with the specific products and systems into which Mini-Circuits' parts are to be incorporated or used so that the proper selection, installation/integration, use and safeguards are made. Accordingly, Mini-Circuits assumes no liability therefor. In addition, your use of this document and the information contained herein is subject to Mini-Circuits' standard terms of use, which are available at Mini-Circuits' website at www.minicircuits.com/homepage/terms_of_use.html.

Mini-Circuits and the Mini-Circuits logo are registered trademarks of Scientific Components Corporation d/b/a Mini-Circuits. All other third-party trademarks are the property of their respective owners. A reference to any third-party trademark does not constitute or imply any endorsement, affiliation, sponsorship, or recommendation: (i) by Mini-Circuits of such third-party's products, services, processes, or other information; or (ii) by any such third-party of Mini-Circuits or its products, services, processes, or other information.